

# Moveout approximation for a converted wave in a moderately anisotropic homogeneous DTI layer

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# Outline

Introduction

Weak-anisotropy parameters

Approximate travelttime formula

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Conclusions

# Introduction

## Moveout approximations

### common

- Taylor series expansion of  $T^2$  in terms of  $x^2$

hyperbolic, non-hyperbolic, ...

### alternative

- expansion of  $T^2$  in terms of the deviations

of anisotropy from isotropy  $\Rightarrow$

weak anisotropy (WA) parameters

# Introduction

## Moveout approximations with WA parameters

- replacement of the actual ray  
by a reference ray in a reference isotropic medium
- approximation of the exact ray velocity  
by the first-order phase velocity
- possible approximate determination of the conversion point  
of the reference ray in the reference medium

# Weak-anisotropy parameters

- 21 weak-anisotropy (WA) parameters  
slightly modified *Mensch & Rasolofosaon (1997)*
- generalization of *Thomsen's (1986)* parameters
- characterize deviations from an isotropic reference
- zero WA parameters → moveout in the isotropic reference medium
- applicable to anisotropy of any type, strength and orientation
- an alternative to stiffness tensor or Voigt's  $C_{\alpha\beta}$  or  $A_{\alpha\beta}$
- can describe exactly any wave attribute

# Weak-anisotropy parameters

- natural combinations of  $C_{\alpha\beta}$  or  $A_{\alpha\beta}$  taken into account
- linear relation of WA to  $C_{\alpha\beta}$  or  $A_{\alpha\beta}$  parameters
- simple linear transformation of WA parameters  
from one coordinate system to another
- definable in coordinate systems independent of symmetry elements  
of studied anisotropy symmetry
- optional choice of the reference velocities  $\alpha, \beta$
- all 21 WA parameters dimensionless, of comparable size

# Weak-anisotropy parameters

$$\epsilon_x = \frac{A_{11}-\alpha^2}{2\alpha^2}, \quad \epsilon_y = \frac{A_{22}-\alpha^2}{2\alpha^2}, \quad \epsilon_z = \frac{A_{33}-\alpha^2}{2\alpha^2}$$

$$\delta_x = \frac{A_{23}+2A_{44}-\alpha^2}{\alpha^2}, \quad \delta_y = \frac{A_{13}+2A_{55}-\alpha^2}{\alpha^2}, \quad \delta_z = \frac{A_{12}+2A_{66}-\alpha^2}{\alpha^2}$$

$$\epsilon_{15} = \frac{A_{15}}{\alpha^2}, \quad \epsilon_{16} = \frac{A_{16}}{\alpha^2}, \quad \epsilon_{24} = \frac{A_{24}}{\alpha^2}, \quad \epsilon_{26} = \frac{A_{26}}{\alpha^2}, \quad \epsilon_{34} = \frac{A_{34}}{\alpha^2}, \quad \epsilon_{35} = \frac{A_{35}}{\alpha^2}$$

$$\chi_x = \frac{A_{14}+2A_{56}}{\alpha^2}, \quad \chi_y = \frac{A_{25}+2A_{46}}{\alpha^2}, \quad \chi_z = \frac{A_{36}+2A_{45}}{\alpha^2}$$

$$\gamma_x = \frac{A_{44}-\beta^2}{2\beta^2}, \quad \gamma_y = \frac{A_{55}-\beta^2}{2\beta^2}, \quad \gamma_z = \frac{A_{66}-\beta^2}{2\beta^2}, \quad \epsilon_{46} = \frac{A_{46}}{\beta^2}, \quad \epsilon_{56} = \frac{A_{56}}{\beta^2}, \quad \epsilon_{45} = \frac{A_{45}}{\beta^2}$$

**DTI WA parameters in the local reflector coordinate system**

$\alpha, \beta$  - P-, S-wave reference velocities

# Weak-anisotropy parameters

**DTI medium**  $(\epsilon_x, \epsilon_z, \delta_y, \gamma_y, \gamma_z)$

WA parameters related to the local reflector coordinate system

$$\epsilon_x = \epsilon_y = \frac{1}{2}\delta_z \quad , \quad \delta_x = \delta_y \quad , \quad \gamma_x = \gamma_y \quad ,$$

$$\epsilon_{15} = \epsilon_{16} = \epsilon_{24} = \epsilon_{26} = \epsilon_{34} = \epsilon_{35} = \epsilon_{45} = \epsilon_{46} = \epsilon_{56} = \chi_x = \chi_y = \chi_z = 0$$



# Weak-anisotropy parameters

Possible use of the estimates of  $\epsilon_x, \epsilon_z, \delta_y, \gamma_y$   
in approximate reconstruction of phase-velocity surfaces:

$$\widetilde{c}_P^2(\mathbf{N}) \sim \alpha^2 \left\{ 1 + 2[\epsilon_x N_1^4 + \delta_y N_1^2 N_3^2 + \epsilon_z N_3^4] \right\}$$

$$\widetilde{c}_{SV}^2(\mathbf{N}) \sim \beta^2 [1 + 2\gamma_y + 2r^{-2}(\epsilon_x + \epsilon_z - \delta_y) N_1^2 N_3^2]$$

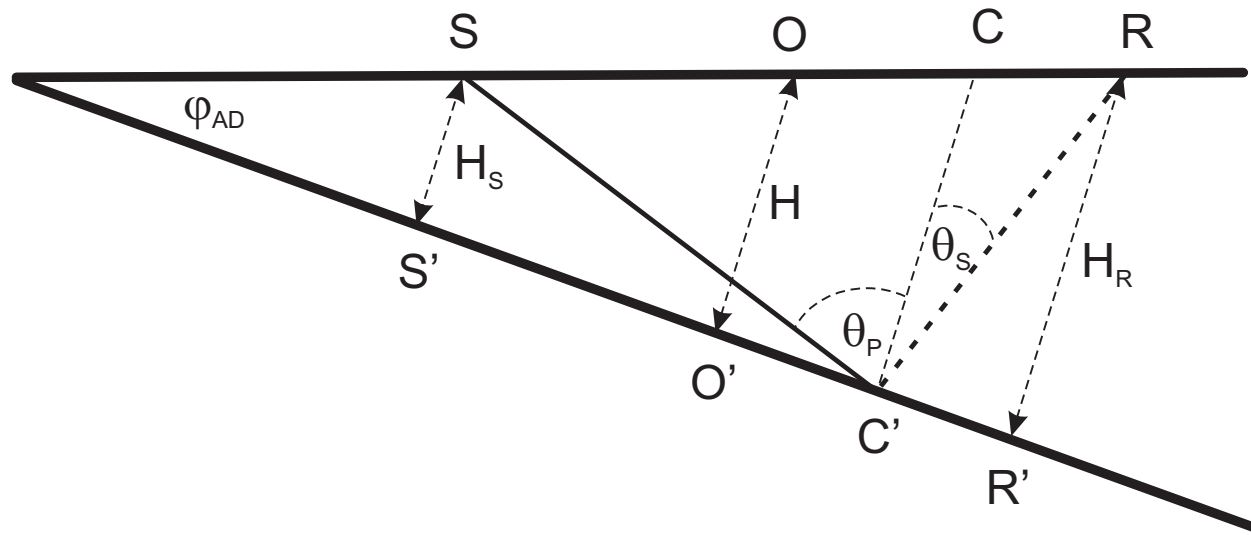
$\widetilde{c}_P^2, \widetilde{c}_{SV}^2$  - approximate squares of P- and S-wave phase velocities

$\alpha, \beta$  - P- and S-wave WA parameters reference velocities

$r = \beta/\alpha$  ,  $\mathbf{N}$  - unit source-receiver vector

# Approximate travelttime formula

## Configuration



$S, R, O, C'$  - source, receiver, midpoint, conversion point

$\overline{SR} \equiv x$  - offset,  $\overline{SC} \equiv x_C$  - offset of the conversion point

$H_S, H_R, H$  - orthogonal distances of  $S, R, O$  from the reflector

$\varphi_{AD}, \theta_P, \theta_S$  - apparent dip angle, angles of incidence and reflection

# Approximate traveltimes formula

## Reflection traveltimes

$$T(x) = T_{HS}(1 + \check{x}_C^2)^{3/2} P_P^{-1/2}(\check{x}_C) + T_{HR}[1 + (\hat{x} - \hat{x}_C)^2]^{3/2} P_{SV}^{-1/2}(\hat{x} - \hat{x}_C)$$

$$T_{HS} = \frac{H_S}{\bar{\alpha}}, \quad T_{HR} = \frac{H_R}{\beta}, \quad \check{x}_C = \frac{x_C \cos \varphi_{AD}}{H_S}, \quad \hat{x} - \hat{x}_C = \frac{(x - x_C) \cos \varphi_{AD}}{H_R}$$

$$P_P(x) = (1 + x^2)^2 + 2\epsilon_x x^4 + 2\delta_y x^2 + 2\epsilon_z$$

$$P_{SV}(x) = (1 + x^2)^2(1 + 2\gamma_y) + 2r^{-2}(\epsilon_x + \epsilon_z - \delta_y)x^2$$

$r = \beta/\alpha$ ;  $\alpha, \beta$  - P- and S-wave WA parameters reference velocities

# Approximate travelttime formula

**Offset of the conversion point  $x_C$   
in a reference isotropic medium:  
solution of the quartic equation**

$$x_C^4 - 2x_C^3x + x_C^2\left(x^2 + \frac{H_R^2\bar{r}^2 - H_S^2}{Q(\bar{r}, \varphi_{AD})}\right) + 2x_C\frac{H_S^2x}{Q(\bar{r}, \varphi_{AD})} - \frac{H_S^2x^2}{Q(\bar{r}, \varphi_{AD})} = 0$$

$x, x_C$  - offset, offset of the conversion point

$$Q(\bar{r}, \varphi_{AD}) = (\bar{r}^2 - 1) \cos^2 \varphi_{AD}$$

$\bar{r} = \bar{\beta}/\bar{\alpha}$ ;  $\bar{\alpha}, \bar{\beta}$  - P- and S-wave reference velocities

$\bar{\alpha}, \bar{\beta}$  may differ from  $\alpha, \beta$  specifying WA parameters

**Determination of  $x_C$ :** exact or approximate (Thomsen, 1999)

# Approximate travelttime formula

## Approximate determination of the conversion point $x_C$

$$x_C \sim x \left[ C_0 + \frac{C_1(x/H) + C_2(x/H)^2}{1 + C_3(x/H)^2} \right]$$

$$C_0 = \frac{1}{1+\bar{r}} , \quad C_1 = -\frac{\bar{r} \sin \varphi_{AD}}{(1+\bar{r})^2} , \quad C_2 = \frac{\bar{r}}{2} \frac{1-\bar{r}}{(1+\bar{r})^3} \cos 2\varphi_{AD} ,$$

$$C_3 = \frac{1}{2} \frac{C_1 |\sin \varphi_{AD}| + 2C_2}{\bar{x}_{Clim} - C_0} - \frac{1}{4} \sin^2 \varphi_{AD}$$

$$\bar{r} = \bar{\beta} / \bar{\alpha} , \quad \bar{x}_{Clim} - \text{limiting value of } x_C , \quad 0 \leq \bar{x}_{Clim} \leq 1$$

### Horizontal reflector

$$C_0 = \frac{1}{1+\bar{r}} , \quad C_1 = 0 , \quad C_2 = \frac{\bar{r}}{2} \frac{1-\bar{r}}{(1+\bar{r})^3} , \quad C_3 = \frac{1}{2} \frac{1-\bar{r}}{(1+\bar{r})^2} \quad \text{Thomsen (1999)}$$

# Tests of formula

## Strength of anisotropy

$$2(c_{max} - c_{min}) / (c_{max} + c_{min}) \times 100\%$$

## Exact reference - ANRAY program package

Relative traveltimes errors:  $(T - T_{ex}) / T_{ex} \times 100\%$

$T$  - approximate traveltimes,  $T_{ex}$  - exact (ANRAY) traveltimes

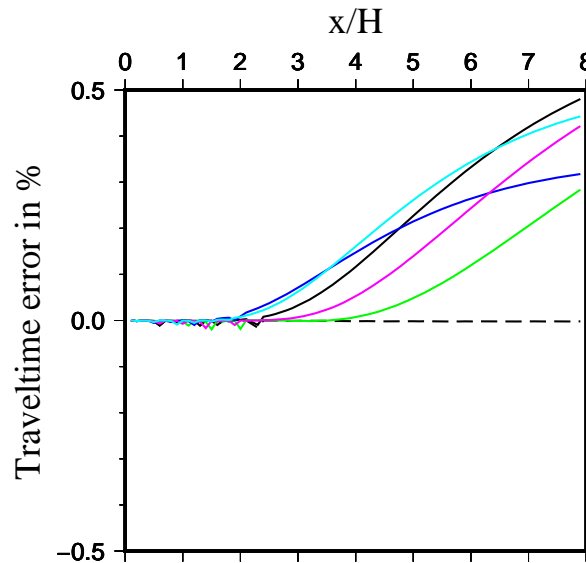
# Tests of formula

**Isotropy ( $\alpha=2.54$  km/s) - horizontal reflector**

$\bar{r} = r = \beta/\alpha = 0.2$  (blue), 0.3 (light blue), 0.4 (black), 0.5 (pink), 0.6 (green)

black dashed curve - WA formula,  $r = 0.4$ ; numerical determination of  $x_C$

coloured solid curves - WA formula, approximate determination of  $x_C$

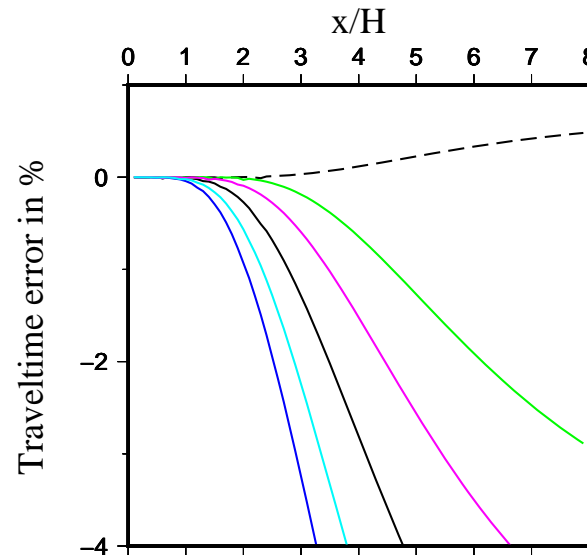


# Tests of formula

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black dashed curve - WA formula,  $r = 0.4$ ; approximate determination of  $x_C$   
coloured solid curves - Tsvankin & Thomsen (1994)

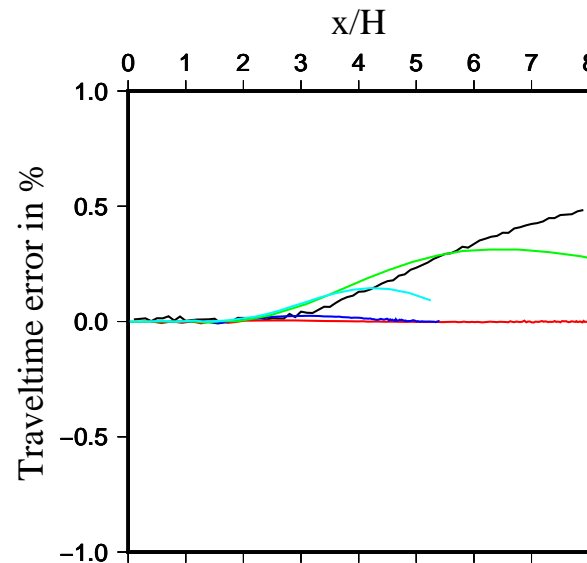




# Tests of formula

**Isotropy ( $\alpha=2.54$  km/s,  $\bar{r} = r=0.4$ ) - dipping reflector**

$\varphi_{AD} = 0^\circ$  (black),  $10^\circ$  (red),  $20^\circ$  (blue),  $-10^\circ$  (green),  $-20^\circ$  (light blue)

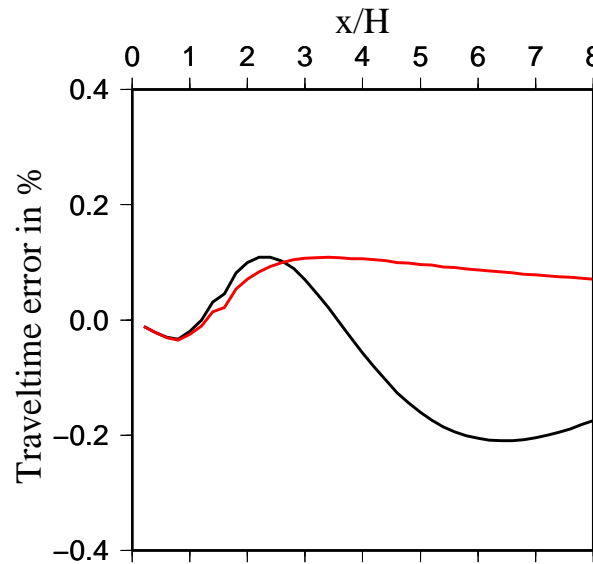


$x_C$  determined from approximate formula (modified Thomsen 1999)

# Tests of formula

**Limestone;  $\sim 8\%$  (P),  $\sim 5\%$  (SV) - horizontal reflector**

$$\epsilon_x=0.076, \quad \delta_y=0.133, \quad \epsilon_z=0, \quad \gamma_y=0, \quad (\bar{r} = r = 0.569)$$



**$x_C$  determined by numerical solution of quadric equation**

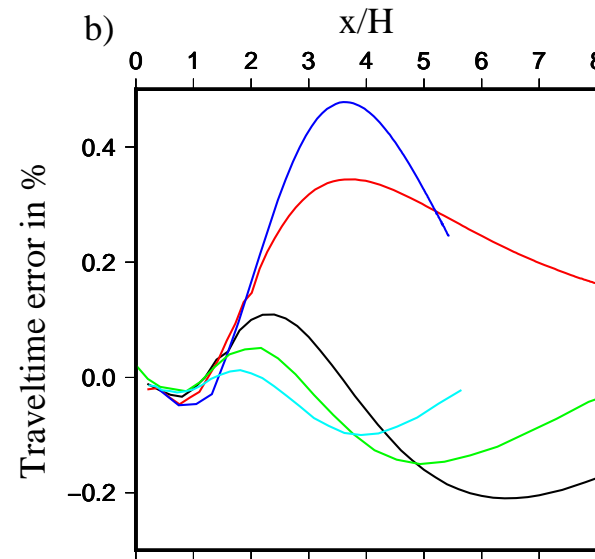
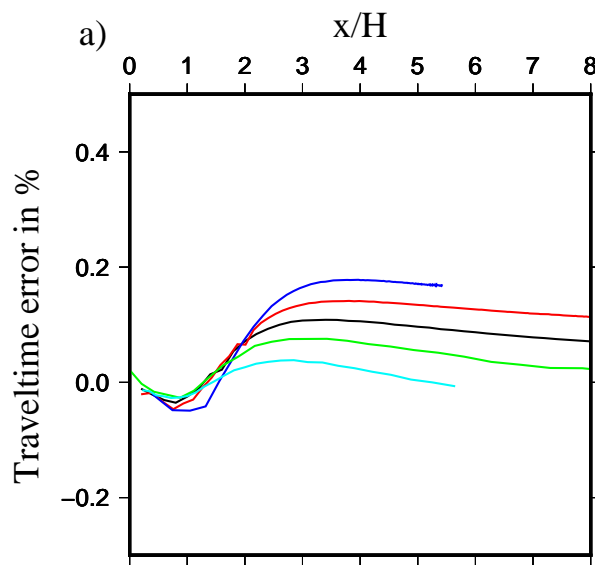
$x_C$  determined from approximate formula of Thomsen (1999)

# Tests of formula

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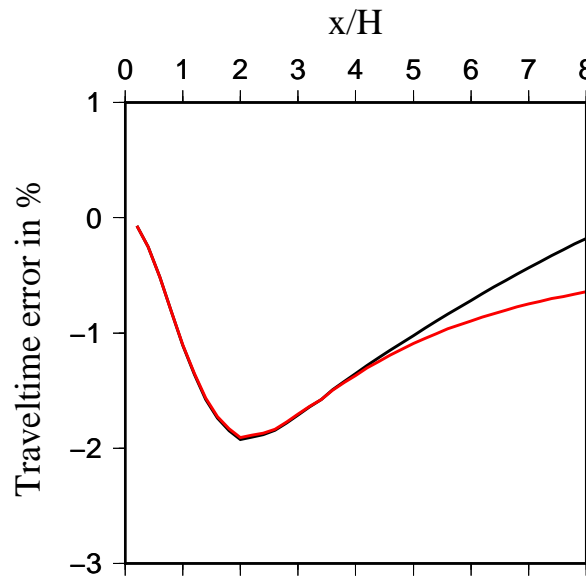


- a)  $x_C$  determined by numerical solution of quadric equation
- b)  $x_C$  determined from approximate formula (modified Thomsen 1999)

# Tests of formula

**Hard shale; ~ 25% (P), ~ 12% (SV) - horizontal reflector**

$$\epsilon_x=0.252, \quad \delta_y=0.034, \quad \epsilon_z=0, \quad \gamma_y=0, \quad (\bar{r} = r = 0.638)$$



**$x_C$  determined by numerical solution of quadric equation**

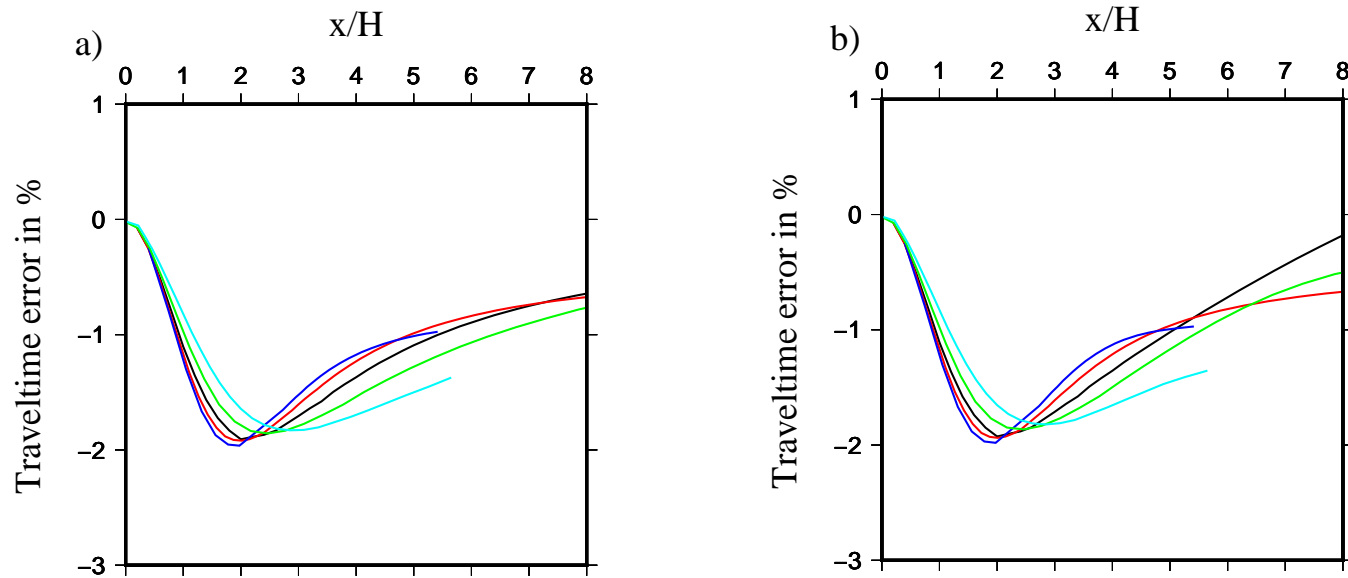
$x_C$  determined from approximate formula of Thomsen (1999)

# Tests of formula

Hard shale;  $\sim 25\%$  (P),  $\sim 12\%$  (SV) - dipping reflector

$$\epsilon_x=0.252, \quad \delta_y=0.034, \quad \epsilon_z=0, \quad \gamma_y=0, \quad (\bar{r} = r = 0.638)$$

$$\varphi_{AD} = 0^\circ \text{ (black)}, 10^\circ \text{ (red)}, 20^\circ \text{ (blue)}, -10^\circ \text{ (green)}, -20^\circ \text{ (light blue)}$$



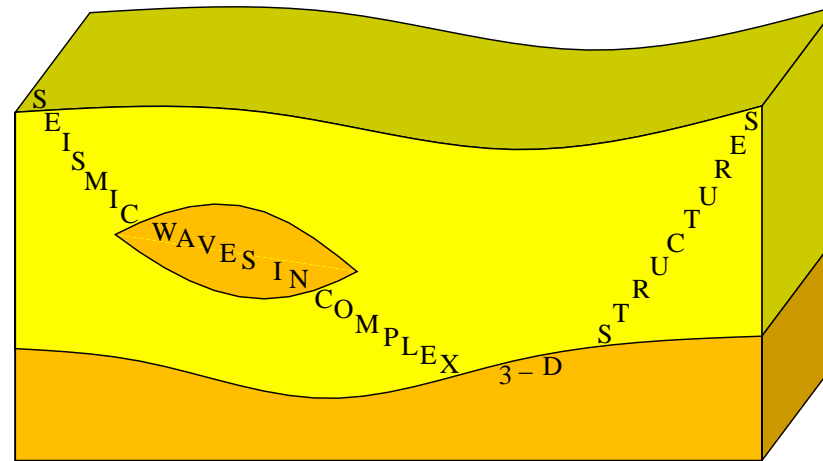
a)  $x_C$  determined by numerical solution of quadric equation

b)  $x_C$  determined from approximate formula (modified Thomsen 1999)

# Conclusions

- moveout formula based on WA approximation
- weak or moderate anisotropy
- simple and transparent, applicable to any offset
- accuracy within the first-order WA approximation
- inaccuracies caused by deviations of  $\mathbf{n}$  and  $\mathbf{N}$
- comparable accuracy with unconverted waves
- formula holds for P-SV as well as SV-P waves
- possible approximate reconstruction of phase-velocity surfaces
- horizontal reflector: possible to express  $T_0$ ,  $v_{NMO}$ ,  $A_4$   
in terms of WA parameters

# Acknowledgement



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